

# DC Motor Speed Control

The original problem is on these web pages.

<http://www.engin.umich.edu/group/ctm/examples/motor/PID2.html>

<http://www.engin.umich.edu/group/ctm/examples/motor2/motor.html>

$$G_m(s) = \frac{\omega(s)}{V(s)} = \frac{K}{(J \cdot s + b) \cdot (L \cdot s + R) + K^2}$$

Transfer function for a DC Motor

$$G_c(s) = \frac{K_i}{s} + K_p + K_d \cdot s$$

A simple PID controller

$$T(s) = \frac{\left( \frac{K_i}{s} + K_p + K_d \cdot s \right) \cdot \frac{K}{(J \cdot s + b) \cdot (L \cdot s + R) + K^2}}{1 + \left( \frac{K_i}{s} + K_p + K_d \cdot s \right) \cdot \frac{K}{(J \cdot s + b) \cdot (L \cdot s + R) + K^2}}$$

Closed loop transfer function

$$T(s) = \frac{G_c(s) \cdot G_m(s)}{1 + G_c(s) \cdot G_m(s)}$$

$$T(s) = \frac{(K_i + K_p \cdot s + K_d \cdot s^2) \cdot K}{J \cdot s^3 \cdot L + (J \cdot R + b \cdot L + K \cdot K_d) \cdot s^2 + (K^2 + K \cdot K_p + b \cdot R) \cdot s + K \cdot K_i}$$

$$T(s) = \frac{(K_i + K_p \cdot s + K_d \cdot s^2) \cdot K}{J \cdot L \cdot s^3 + \frac{J \cdot R + b \cdot L + K \cdot K_d}{J \cdot L} \cdot s^2 + \frac{K^2 + K \cdot K_p + b \cdot R}{J \cdot L} \cdot s + \frac{K \cdot K_i}{J \cdot L}}$$

$$(s + \lambda)^3$$

Desired characteristic equation. In this case a critically damped response is desired with 3 poles at  $-\lambda$ .

Find the difference between the system characteristic equation and the desired characteristic equation and solve for the gains.

$$\text{DiffCE} := s^3 + \frac{J \cdot R + b \cdot L + K \cdot K_d}{J \cdot L} \cdot s^2 + \frac{K^2 + K \cdot K_p + b \cdot R}{J \cdot L} \cdot s + \frac{K \cdot K_i}{J \cdot L} - (s + \lambda)^3$$

$$\text{DiffCE} \left| \begin{array}{l} \text{coeffs}, s \\ \text{solve}, \begin{pmatrix} K_i \\ K_p \\ K_d \end{pmatrix} \end{array} \right. \rightarrow \left[ \lambda^3 \cdot J \cdot \frac{L}{K} \quad \frac{(-K^2) - b \cdot R + 3 \cdot \lambda^2 \cdot J \cdot L}{K} \quad \frac{(-J) \cdot R - b \cdot L + 3 \cdot \lambda \cdot J \cdot L}{K} \right]$$

# DC Motor Speed Control

## DC Motor Parameters

See <http://www.engin.umich.edu/group/ctm/examples/motor/motor.html>

$J := 0.01$	$J = 0.01$	kg*m <sup>2</sup>
$b := 0.1$	$b = 0.1$	N*m*s
$K := 0.01$	$K = 0.01$	V/rad/sec
$R := 1$	$R = 1$	Ohm
$L := 0.5$	$L = 0.5$	Henrys

Find the DC gain. It is about 0.1 radians per second per volt. Therefore the motor has a maximum speed of 1 radian per second which is very slow. Obviously this is not a realistic example.

$$\lim_{s \rightarrow 0} \frac{K}{(J \cdot s + b) \cdot (L \cdot s + R) + K^2} \text{ float, 2 } \rightarrow .10$$

Calculate the PID gains. Place the three closed loop poles at  $-\lambda$  radians to get a critically damped response. Making  $\lambda$  bigger moves the closed loop poles farther to the left and makes the response faster.

$\lambda := 2 \cdot \pi \cdot 3$	$\lambda = 18.849556$
$K_i := \lambda^3 \cdot J \cdot \frac{L}{K}$	$K_i = 3348.677881$
$K_p := \frac{(-K^2) - b \cdot R + 3 \cdot \lambda^2 \cdot J \cdot L}{K}$	$K_p = 522.948638$
$K_d := \frac{(-J) \cdot R - b \cdot L + 3 \cdot \lambda \cdot J \cdot L}{K}$	$K_d = 22.274334$

# DC Motor Speed Control

## Simulate modeling errors

The rnorm function generates a number with a mean of 1 and a standard deviation of  $\sigma$ . These numbers multiplied by the model parameters to generate simulated 'true' systems parameters.

$$\sigma := 0.1$$

$$K := K \cdot \text{rnorm}(1, 1, \sigma)_0 \quad K = 0.01$$

$$J := J \cdot \text{rnorm}(1, 1, \sigma)_0 \quad J = 0.01$$

$$b := b \cdot \text{rnorm}(1, 1, \sigma)_0 \quad b = 0.1$$

$$R := R \cdot \text{rnorm}(1, 1, \sigma)_0 \quad R = 1$$

$$L := L \cdot \text{rnorm}(1, 1, \sigma)_0 \quad L = 0.5$$

## The DC Motor Velocity Model in State Space

$$A_c := \begin{pmatrix} -\frac{b}{J} & \frac{K}{J} \\ -\frac{K}{L} & -\frac{R}{L} \end{pmatrix} \quad A_c = \begin{pmatrix} -10 & 1 \\ -0.02 & -2 \end{pmatrix} \quad B_c := \begin{pmatrix} 0 \\ \frac{1}{L} \end{pmatrix} \quad B_c = \begin{pmatrix} 0 \\ 2 \end{pmatrix}$$

$$I := \text{identity}(2)$$

$$T := .001$$

Calculate arrays for use in discrete time.

$$A := I + \sum_{n=1}^7 \frac{(A_c \cdot T)^n}{n!} \quad B := \left[ I + \sum_{n=1}^7 \frac{(A_c \cdot T)^n}{(n+1)!} \right] \cdot B_c \cdot T$$

$$A = \begin{pmatrix} 0.99005 & 0.000994 \\ -0.00002 & 0.998002 \end{pmatrix} \quad B = \begin{pmatrix} 9.960103 \times 10^{-7} \\ 0.001998 \end{pmatrix}$$

$$Kz_i := (K_i \quad K_p \quad K_d) \cdot \begin{pmatrix} T & 0 & 0 \\ 1 & -1 & 0 \\ \frac{1}{T} & -\frac{2}{T} & \frac{1}{T} \end{pmatrix}$$

Convert the PID gains to coefficients for the PID difference equation.

$$Kz_i = (22800.631198 \quad -45071.616402 \quad 22274.333882)$$

# DC Motor Speed Control

PID Critically Damped Control. Graph the response of the DC Motor

$$x_0 := \begin{pmatrix} 0 \\ 0 \end{pmatrix} \quad u_0 := 0 \quad \text{err}_0 := \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

$$\text{PID}(r, x, u, \text{err}) := \left( \begin{array}{l} \text{err} \leftarrow \begin{pmatrix} r - x_0 \\ \text{err}_0 \\ \text{err}_1 \end{pmatrix} \\ \begin{pmatrix} A \cdot x + B \cdot u \\ \max(\min(u + K_{Z1} \cdot \text{err}, 10), -10) \\ \text{err} \end{pmatrix} \end{array} \right)$$

Shift the error history  
Update state  
Calculate control output  
Return the error history too

Simulate 10 seconds in increments of T seconds

$$N := \frac{10}{T} \quad N = 10000 \quad n := 0..N$$

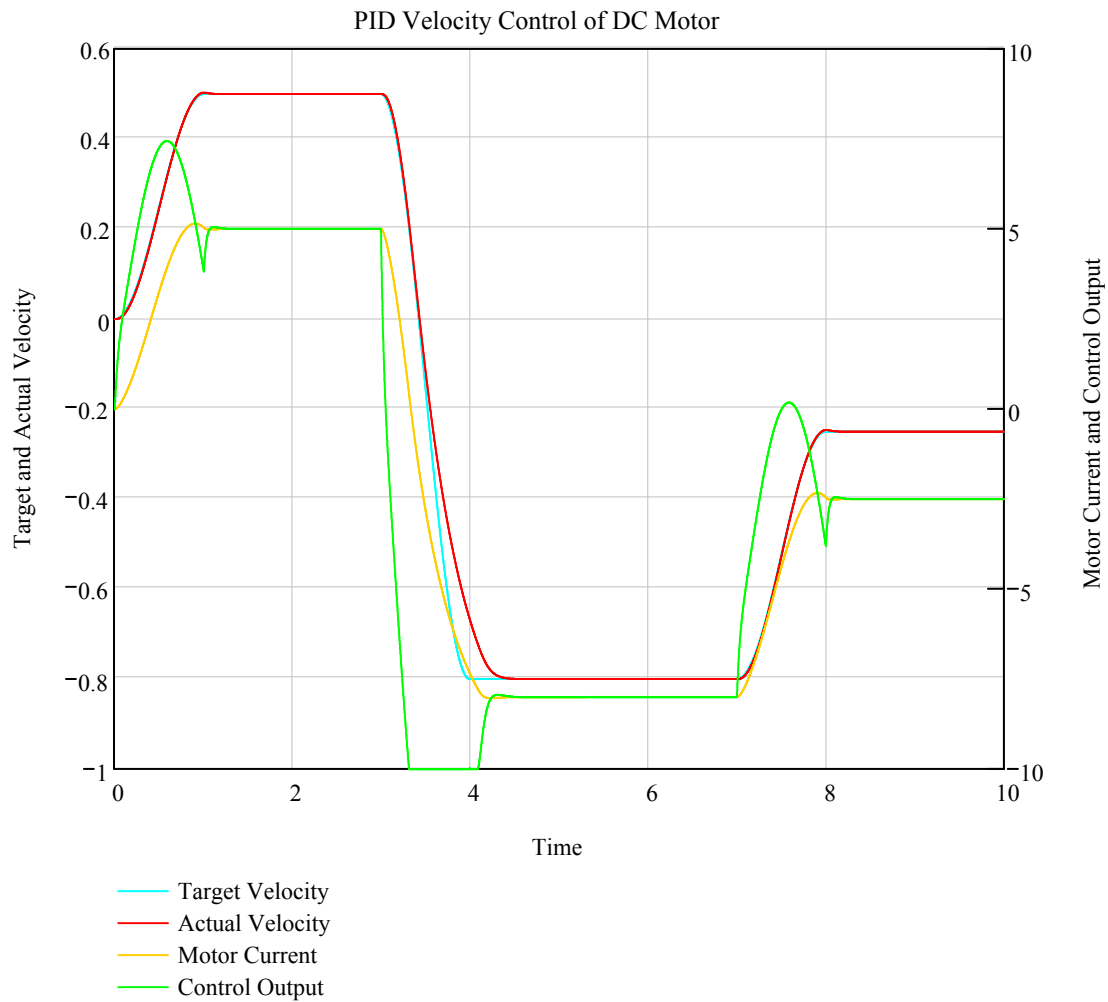
$$r_n := \begin{cases} 0 & \text{if } n < 10 \\ \left( \frac{0.5 + 0.0}{2} \right) - \left( \frac{0.5 - 0.0}{2} \right) \cdot \cos \left[ \pi \cdot \left( \frac{n - 10}{0.1 \cdot N} \right) \right] & \text{if } 10 \leq n < 1010 \\ 0.5 & \text{if } n \geq 1010 \wedge n < 0.3 \cdot N \\ \left( \frac{0.5 - 0.8}{2} \right) - \left[ \left( \frac{-0.8 - 0.5}{2} \right) \cdot \cos \left[ \pi \cdot \left( \frac{n - 0.3 \cdot N}{0.1 \cdot N} \right) \right] \right] & \text{if } 0.3 \cdot N \leq n < 0.4 \cdot N \\ -0.8 & \text{if } n \geq 0.4 \cdot N \wedge n < 0.7 \cdot N \\ \left( \frac{-0.8 - 0.25}{2} \right) - \left[ \left( \frac{-0.25 - -0.8}{2} \right) \cdot \cos \left[ \pi \cdot \left( \frac{n - 0.7 \cdot N}{0.1 \cdot N} \right) \right] \right] & \text{if } 0.7 \cdot N \leq n < 0.8 \cdot N \\ -0.25 & \text{otherwise} \end{cases}$$

r(n) is the target or reference velocity.

$$\begin{pmatrix} x_{n+1} \\ u_{n+1} \\ \text{err}_{n+1} \end{pmatrix} := \text{PID}(r_n, x_n, u_n, \text{err}_n)$$

Call the PID routine for each time period.

# DC Motor Speed Control



$K = 0.01$	$J = 0.01$	$R = 1$	$L = 0.5$	Motor
$\lambda = 18.849556$	$K_i = 3348.677881$	$K_p = 522.948638$	$K_d = 22.274334$	Inner Loop

The actual velocity tracks the target velocity almost perfectly except where the control output saturates at about 3.3 seconds. A less radical velocity change or reducing the bandwidth by reducing  $\lambda$  would avoid the output saturation.

# DC Motor Speed Control

## Open Loop Bode Plot Calculations

$$T(s) := \left( \frac{K_i}{s} + K_p + K_d \cdot s \right) \cdot \frac{K}{(J \cdot s + b) \cdot (L \cdot s + R) + K^2}$$

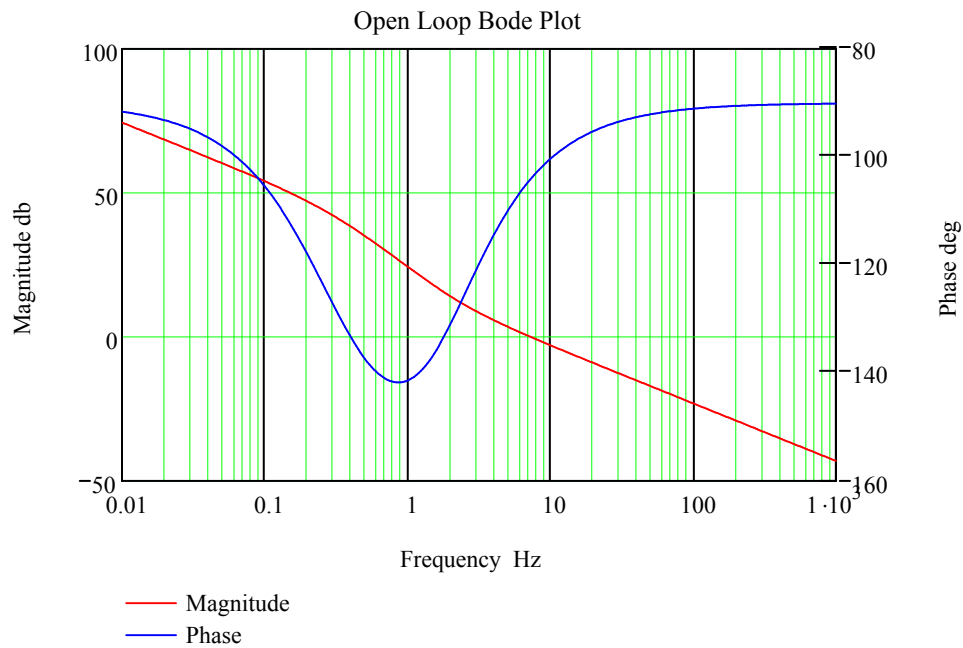
$n := 0..320$

Iterate the frequency from .01 HZ to 1000 HZ using 64 steps per decade for a total of 256 iterations.

$$Hz_n := 10^{\frac{n}{64} - 2}$$

Closed loop magnitude of transfer function as a function of frequency

$$\begin{pmatrix} M_n \\ \phi_n \end{pmatrix} := \begin{cases} r \leftarrow T[j \cdot (2 \cdot \pi) \cdot Hz_n] \\ a \leftarrow \frac{\arg(r)}{\deg} \\ a \leftarrow a - 360 \text{ if } n > 0 \wedge |a - \phi_{n-1}| > 100 \\ \begin{pmatrix} 20 \cdot \log(|r|) \\ a \end{pmatrix} \end{cases}$$



# DC Motor Speed Control

## Closed Loop Bode Plot Calculations

$$T(s) := \frac{(K_i + K_p \cdot s + K_d \cdot s^2) \cdot K}{J \cdot s^3 \cdot L + J \cdot s^2 \cdot R + b \cdot L \cdot s^2 + s \cdot b \cdot R + s \cdot K^2 + K \cdot K_i + K \cdot K_p \cdot s + K \cdot K_d \cdot s^2}$$

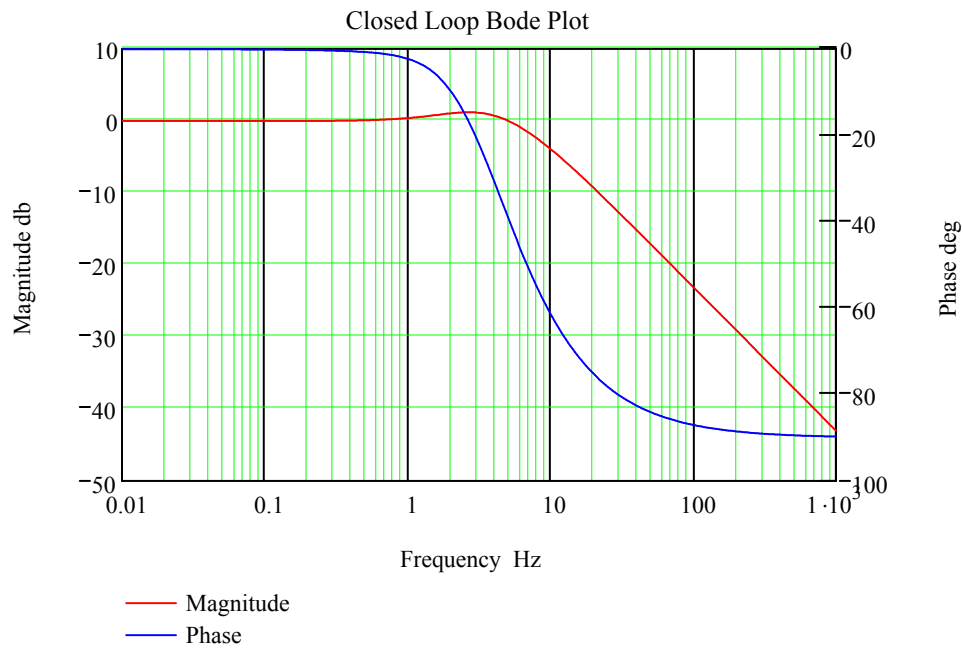
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# DC Motor Speed Control

## Poles and Zeros

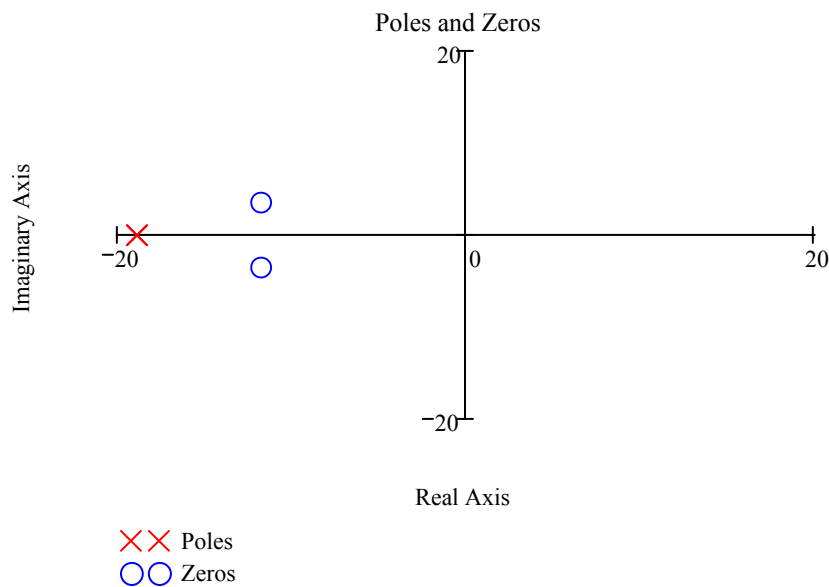
$$T(s) := \frac{(K_i + K_p \cdot s + K_d \cdot s^2) \cdot K}{J \cdot s^3 \cdot L + (J \cdot R + b \cdot L + K \cdot K_d) \cdot s^2 + (K^2 + K \cdot K_p + b \cdot R) \cdot s + K \cdot K_i}$$

$$J \cdot s^3 \cdot L + (J \cdot R + b \cdot L + K \cdot K_d) \cdot s^2 + (K^2 + K \cdot K_p + b \cdot R) \cdot s + K \cdot K_i \quad \left| \begin{array}{l} \text{coeffs, s} \\ \text{explicit} \end{array} \right. \rightarrow \begin{pmatrix} K \cdot K_i \\ K^2 + K \cdot K_p + b \cdot R \\ J \cdot R + b \cdot L + K \cdot K_d \\ J \cdot L \end{pmatrix}$$

$$\text{poles} := \text{polyroots} \left( \begin{pmatrix} K \cdot K_i \\ K^2 + K \cdot K_p + b \cdot R \\ J \cdot R + b \cdot L + K \cdot K_d \\ J \cdot L \end{pmatrix} \right) \quad \text{poles} = \begin{pmatrix} -18.849556 \\ -18.849556 \\ -18.849555 \end{pmatrix} \quad \text{Right where we wanted them to be!}$$

$$(K_i + K_p \cdot s + K_d \cdot s^2) \cdot K \quad \left| \begin{array}{l} \text{coeffs, s} \\ \text{explicit} \end{array} \right. \rightarrow \begin{pmatrix} K \cdot K_i \\ K \cdot K_p \\ K \cdot K_d \end{pmatrix}$$

$$\text{zeros} := \text{polyroots} \left( \begin{pmatrix} K \cdot K_i \\ K \cdot K_p \\ K \cdot K_d \end{pmatrix} \right) \quad \text{zeros} = \begin{pmatrix} -11.738817 - 3.540924i \\ -11.738817 + 3.540924i \end{pmatrix}$$





# DC Motor Speed Control

## Add Outer Position Loop

$$\lambda := \lambda \quad K_{i_1} := K_i \quad K_{p_1} := K_p \quad K_{d_1} := K_d$$

Use i subscripts for inner loop parameters and i subscripts for outer loop parameters.

$$T_o = \frac{\left( \frac{K_{i_o}}{s} + K_{p_o} + K_{d_o} \cdot s \right) \cdot \frac{\lambda^3}{s \cdot (s + \lambda)^3}}{1 + \left( \frac{K_{i_o}}{s} + K_{p_o} + K_{d_o} \cdot s \right) \cdot \frac{\lambda^3}{s \cdot (s + \lambda)^3}}$$

$$T_o = \frac{(K_{i_o} + K_{p_o} \cdot s + K_{d_o} \cdot s^2) \cdot \lambda^3}{s^5 + 3 \cdot s^4 \cdot \lambda + 3 \cdot s^3 \cdot \lambda^2 + (\lambda^3 \cdot K_{d_o} + \lambda^3) \cdot s^2 + \lambda^3 \cdot K_{p_o} \cdot s + \lambda^3 \cdot K_{i_o}}$$

$$\text{DiffCE} := s^5 + 3 \cdot s^4 \cdot \lambda + 3 \cdot s^3 \cdot \lambda^2 + (\lambda^3 \cdot K_{d_o} + \lambda^3) \cdot s^2 + \lambda^3 \cdot K_{p_o} \cdot s + \lambda^3 \cdot K_{i_o} - (s + \mu)^3 \cdot (s + \alpha) \cdot (s + \beta)$$

$$\text{DiffCE} \left| \begin{array}{l} \text{coeffs, s} \\ \text{solve, } \begin{pmatrix} K_{i_o} \\ K_{p_o} \\ K_{d_o} \\ \alpha \\ \beta \end{pmatrix} \end{array} \right. \rightarrow \left[ \begin{array}{ccc} 3 \cdot \mu^3 \cdot \frac{\lambda^2 - 3 \cdot \mu \cdot \lambda + 2 \cdot \mu^2}{\lambda^3} & 3 \cdot \mu^2 \cdot \frac{(-8) \cdot \mu \cdot \lambda + 5 \cdot \mu^2 + 3 \cdot \lambda^2}{\lambda^3} & \frac{-(\lambda^3 + 18 \cdot \mu^2 \cdot \lambda - 10 \cdot \mu^3)}{\lambda^3} \\ 3 \cdot \mu^3 \cdot \frac{\lambda^2 - 3 \cdot \mu \cdot \lambda + 2 \cdot \mu^2}{\lambda^3} & 3 \cdot \mu^2 \cdot \frac{(-8) \cdot \mu \cdot \lambda + 5 \cdot \mu^2 + 3 \cdot \lambda^2}{\lambda^3} & \frac{-(\lambda^3 + 18 \cdot \mu^2 \cdot \lambda - 10 \cdot \mu^3)}{\lambda^3} \end{array} \right]$$

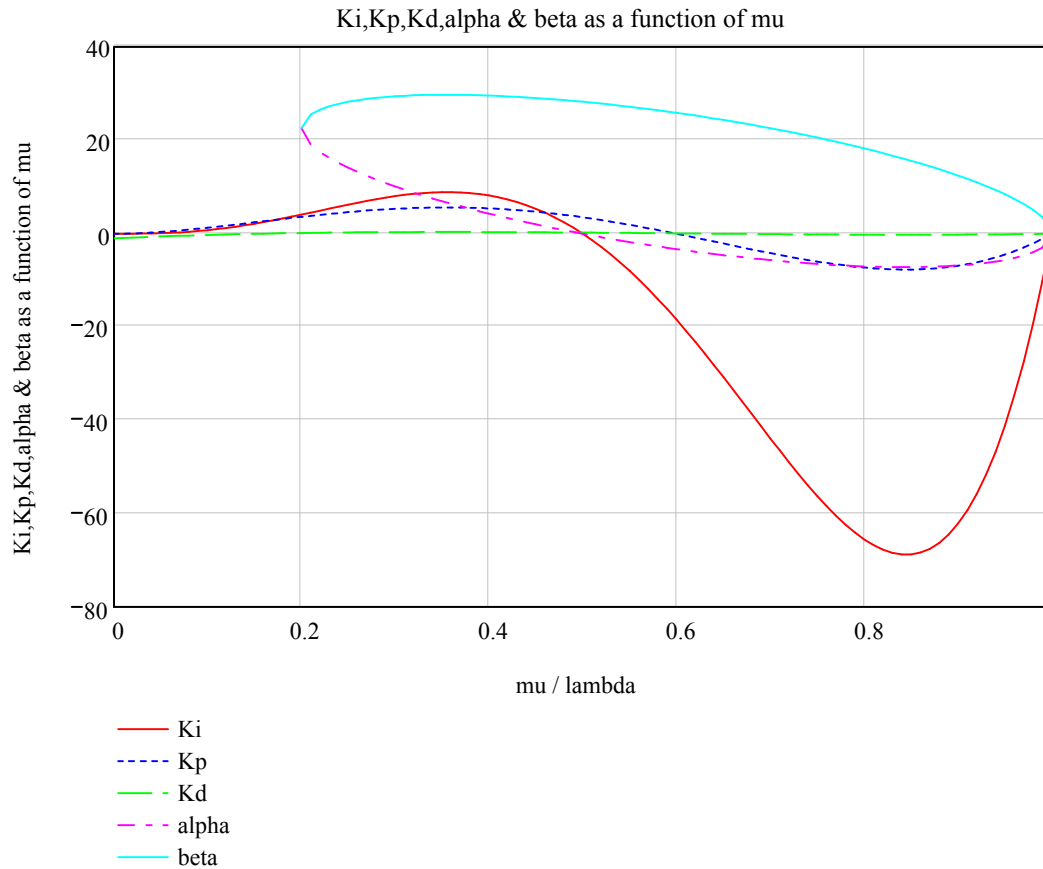
$$\begin{pmatrix} K_{i_o} \\ K_{p_o} \\ K_{d_o} \\ \alpha \\ \beta \end{pmatrix} = \left[ \begin{array}{c} 3 \cdot \mu^3 \cdot \frac{\lambda^2 - 3 \cdot \mu \cdot \lambda + 2 \cdot \mu^2}{\lambda^3} \\ 3 \cdot \mu^2 \cdot \frac{5 \cdot \mu^2 - 8 \cdot \mu \cdot \lambda + 3 \cdot \lambda^2}{\lambda^3} \\ \frac{10 \cdot \mu^3 - 18 \cdot \mu^2 \cdot \lambda - \lambda^3 + 9 \cdot \mu \cdot \lambda^2}{\lambda^3} \\ \frac{3}{2} \cdot \lambda - \frac{3}{2} \cdot \mu - \frac{1}{2} \cdot [(-3) \cdot \lambda^2 + 18 \cdot \mu \cdot \lambda - 15 \cdot \mu^2]^{\frac{1}{2}} \\ \frac{3}{2} \cdot \lambda - \frac{3}{2} \cdot \mu + \frac{1}{2} \cdot [(-3) \cdot \lambda^2 + 18 \cdot \mu \cdot \lambda - 15 \cdot \mu^2]^{\frac{1}{2}} \end{array} \right]$$

The symbolic equations for the outer loop gains as a function of the inner loop poles and the outer loop poles. If the relationship between the outer loop poles,  $\mu$ , and the inner loop poles,  $\lambda$ , is not right the outer loop gains will be negative or the unplaced poles,  $\alpha$  and  $\beta$ , will be in the right hand plane.

# DC Motor Speed Control

Graphs the outer loop gains and  $\alpha$  and  $\beta$  as a function of the ratio of the outer loop pole location to the inner loop pole locations. This is backwards from a root locus plot.

$$\mu := 0, 0.01\lambda \dots 1\lambda$$



$\mu$  is only valid where  $K_i$ ,  $K_p$ ,  $K_d$ ,  $\alpha$  and  $\beta$  are positive and this is only a small fractional range of  $\lambda$ .

$K_d$  is negative if  $\mu/\lambda$  is too low and  $\alpha$  and  $\beta$  are negative if  $\mu/\lambda$  is greater than 1.

$K_i$ ,  $K_p$  and  $K_d$  are maximum at  $0.355\lambda$ :

# DC Motor Speed Control

$\mu := \mu$

Find  $\mu$  for max  $K_i$

$$\frac{d}{d\mu} \left( 3 \cdot \mu^3 \cdot \frac{\lambda^2 - 3 \cdot \mu \cdot \lambda + 2 \cdot \mu^2}{\lambda^3} \right) \text{ solve, } \mu \rightarrow \begin{bmatrix} 0 \\ 0 \\ \left( \frac{3}{5} + \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \\ \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ \left( \frac{3}{5} + \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \\ \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \end{bmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0.844949 \\ 0.355051 \end{pmatrix}$$

Find  $\mu$  for max  $K_p$

$$\frac{d}{d\mu} \left( 3 \cdot \mu^2 \cdot \frac{5 \cdot \mu^2 - 8 \cdot \mu \cdot \lambda + 3 \cdot \lambda^2}{\lambda^3} \right) \text{ solve, } \mu \rightarrow \begin{bmatrix} 0 \\ \left( \frac{3}{5} + \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \\ \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \end{bmatrix} \begin{bmatrix} 0 \\ \left( \frac{3}{5} + \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \\ \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \end{bmatrix} = \begin{pmatrix} 0 \\ 15.926913 \\ 6.692554 \end{pmatrix}$$

Find  $\mu$  for max  $K_d$

$$\frac{d}{d\mu} \left( 3 \cdot \frac{10 \cdot \mu^3 - 18 \cdot \mu^2 \cdot \lambda - \lambda^3 + 9 \cdot \mu \cdot \lambda^2}{\lambda^3} \right) \text{ solve, } \mu \rightarrow \begin{bmatrix} \left( \frac{3}{5} + \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \\ \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \end{bmatrix}$$

The maximum outer loop gains will all happen at the same ratio of  $\mu$  to  $\lambda$ .

$$\mu := \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \text{ or about } 0.355 \cdot \lambda$$

$$\mu := \left( \frac{3}{5} + \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda \quad \mu = 6.692554$$

## DC Motor Speed Control

Substitute the optimal value of  $\mu$  in terms of  $\lambda$

Now all tuning can be done in terms of the inner loop poles position using  $\lambda$  alone.

$$\begin{pmatrix} K_{i_o} \\ K_{p_o} \\ K_{d_o} \\ \alpha \\ \beta \end{pmatrix} = \begin{bmatrix} 3 \cdot \mu^3 \cdot \frac{\lambda^2 - 3 \cdot \mu \cdot \lambda + 2 \cdot \mu^2}{\lambda^3} \\ 3 \cdot \mu^2 \cdot \frac{5 \cdot \mu^2 - 8 \cdot \mu \cdot \lambda + 3 \cdot \lambda^2}{\lambda^3} \\ \frac{10 \cdot \mu^3 - 18 \cdot \mu^2 \cdot \lambda - \lambda^3 + 9 \cdot \mu \cdot \lambda^2}{\lambda^3} \\ \frac{3}{2} \cdot \lambda - \frac{3}{2} \cdot \mu - \frac{1}{2} \cdot [(-3) \cdot \lambda^2 + 18 \cdot \mu \cdot \lambda - 15 \cdot \mu^2]^{\frac{1}{2}} \\ \frac{3}{2} \cdot \lambda - \frac{3}{2} \cdot \mu + \frac{1}{2} \cdot [(-3) \cdot \lambda^2 + 18 \cdot \mu \cdot \lambda - 15 \cdot \mu^2]^{\frac{1}{2}} \end{bmatrix}$$

substitute,  $\mu = \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda$

expand

simplify

collect,  $\lambda$

$\rightarrow \begin{pmatrix} K_{i_o} \\ K_{p_o} \\ K_{d_o} \\ \alpha \\ \beta \end{pmatrix} =$

## DC Motor Speed Control

The formulas for outer loop gains and unplaced poles in terms of  $\lambda$  alone

$$\begin{pmatrix} K_{i_o} \\ K_{p_o} \\ K_{d_o} \\ \alpha \\ \beta \end{pmatrix} = \begin{bmatrix} 3 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^3 \cdot \left[ \frac{-4}{5} + \frac{3}{10} \cdot 6^{\frac{1}{2}} + 2 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 \right] \cdot \lambda^2 \\ 3 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 \cdot \left[ 5 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 - \frac{9}{5} + \frac{4}{5} \cdot 6^{\frac{1}{2}} \right] \cdot \lambda \\ 10 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^3 - 18 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 + \frac{22}{5} - \frac{9}{10} \cdot 6^{\frac{1}{2}} \\ \left( \frac{3}{5} + \frac{3}{20} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda - \frac{1}{2} \cdot \left[ (-3) \cdot \lambda^2 + 18 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda^2 - 15 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 \cdot \lambda^2 \right]^{\frac{1}{2}} \\ \left( \frac{3}{5} + \frac{3}{20} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda + \frac{1}{2} \cdot \left[ (-3) \cdot \lambda^2 + 18 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda^2 - 15 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 \cdot \lambda^2 \right]^{\frac{1}{2}} \end{bmatrix}$$

# DC Motor Speed Control

Calculate numerical values for the outer loop gains

$$\lambda = 18.849556$$

$$\mu := 0.45 \cdot \lambda$$

$$\mu = 6.692554$$

Three Inner loop poles at  $-\lambda$

Enable to override optimum outer loop gains.

Three Outer loop poles at  $-\mu$

$$\begin{pmatrix} K_{i_o} \\ K_{p_o} \\ K_{d_o} \\ \alpha \\ \beta \end{pmatrix} := \begin{pmatrix} 3 \cdot \mu^3 \cdot \frac{\lambda^2 - 3 \cdot \mu \cdot \lambda + 2 \cdot \mu^2}{\lambda^3} \\ 3 \cdot \mu^2 \cdot \frac{5 \cdot \mu^2 - 8 \cdot \mu \cdot \lambda + 3 \cdot \lambda^2}{\lambda^3} \\ \frac{10 \cdot \mu^3 - 18 \cdot \mu^2 \cdot \lambda - \lambda^3 + 9 \cdot \mu \cdot \lambda^2}{\lambda^3} \\ \frac{3}{2} \cdot \lambda - \frac{3}{2} \cdot \mu - \frac{1}{2} \cdot \left[ (-3) \cdot \lambda^2 + 18 \cdot \mu \cdot \lambda - 15 \cdot \mu^2 \right]^{\frac{1}{2}} \\ \frac{3}{2} \cdot \lambda - \frac{3}{2} \cdot \mu + \frac{1}{2} \cdot \left[ (-3) \cdot \lambda^2 + 18 \cdot \mu \cdot \lambda - 15 \cdot \mu^2 \right]^{\frac{1}{2}} \end{pmatrix}$$

$$\begin{pmatrix} K_{i_o} \\ K_{p_o} \\ K_{d_o} \\ \alpha \\ \beta \end{pmatrix} = \begin{pmatrix} 8.92003 \\ 5.630862 \\ 0.373939 \\ 6.692554 \\ 29.778451 \end{pmatrix}$$

$\alpha$  is the same as  $\mu$  so there are four outer loop poles at  $\mu$  and one at  $\beta$ . The pole at  $\beta$  is always farther to the left so it doesn't affect the response much.

# DC Motor Speed Control

The DC Motor Velocity Model in State Space

$$A_c := \begin{pmatrix} 0 & 1 & 0 \\ 0 & -\frac{b}{J} & \frac{K}{J} \\ 0 & -\frac{K}{L} & -\frac{R}{L} \end{pmatrix} \quad A_c = \begin{pmatrix} 0 & 1 & 0 \\ 0 & -10 & 1 \\ 0 & -0.02 & -2 \end{pmatrix} \quad B_c := \begin{pmatrix} 0 \\ 0 \\ \frac{1}{L} \end{pmatrix} \quad B_c = \begin{pmatrix} 0 \\ 0 \\ 2 \end{pmatrix}$$

$I := \text{identity}(3)$

Calculate arrays for use in discrete time.

$$A := I + \sum_{n=1}^7 \frac{(A_c \cdot T)^n}{n!} \quad B := \left[ I + \sum_{n=1}^7 \frac{(A_c \cdot T)^n}{(n+1)!} \right] \cdot B_c \cdot T$$

$$A = \begin{pmatrix} 1 & 0.000995 & 4.980052 \times 10^{-7} \\ 0 & 0.99005 & 0.000994 \\ 0 & -0.00002 & 0.998002 \end{pmatrix} \quad B = \begin{pmatrix} 3.323354 \times 10^{-10} \\ 9.960103 \times 10^{-7} \\ 0.001998 \end{pmatrix}$$

# DC Motor Speed Control

## Cascade Control

The Cascaded loop controller and system simulator.

An outer loop closed loop generates a reference velocity. The inner loop tries to follow the velocity generated by the outer loop.

Note the outer and inner loop is really using I-PD control where only the integrator term is in the forward path. This makes the inner loop less susceptible to the noise in the set point from the outer loop.

The second line computes the control output using the error between velocity generated from the outer loop and the feed back or estimated velocity. The control output is limited to -10 to +10 volts

$$N := \frac{10}{T} \quad n := 0..N$$

Simulate 10  
seconds

$$r_n := \begin{cases} x_0 & \text{if } n < 0.01 \cdot N \\ \begin{pmatrix} 0.2 \\ 0 \end{pmatrix} & \text{if } 0.01 \cdot N \leq n \wedge n < 0.2 \cdot N \\ \begin{pmatrix} 0.1 \\ 0 \end{pmatrix} & \text{if } 0.2 \cdot N \leq n \wedge n < 0.4 \cdot N \\ \begin{pmatrix} 0.05 \\ 0 \end{pmatrix} & \text{if } 0.4 \cdot N \leq n \wedge n < 0.65 \cdot N \\ \begin{pmatrix} 0.35 \\ 0 \end{pmatrix} & \text{otherwise} \end{cases}$$

Calculate the target positions and velocities. In this case the target velocities are 0 since that target positions are changing only in step jumps.



# DC Motor Speed Control

```

Cascade(r) := 
$$\begin{array}{l} x_0 \leftarrow \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix} \\ v_0 \leftarrow 0 \\ v_i \leftarrow 0 \\ u_0 \leftarrow 0 \\ u_i \leftarrow 0 \\ \text{for } n \in 0..N-1 \\ \quad \left| \begin{array}{l} x_{n+1} \leftarrow A \cdot x_n + B \cdot u_n \\ v_{pd} \leftarrow -\left[ K_{p_o} \cdot (x_{n+1})_0 + \frac{K_{d_o}}{T} \cdot \left[ (x_{n+1})_0 - (x_n)_0 \right] \right] \\ v_i \leftarrow \max \left[ \min \left[ v_i + K_{i_o} \cdot T \cdot \left[ (r_{n+1})_0 - (x_{n+1})_0 \right], 1.0 - v_{pd} \right], -1.0 - v_{pd} \right] \\ v_{n+1} \leftarrow v_i + v_{pd} \\ u_{pd} \leftarrow -\left[ K_{p_i} \cdot (x_{n+1})_1 + \frac{K_{d_i}}{T} \cdot \left[ (x_{n+1})_1 - (x_n)_1 \right] \right] \\ u_i \leftarrow \max \left[ \min \left[ u_i + K_{i_i} \cdot T \cdot \left[ v_{n+1} - (x_{n+1})_1 \right], 10 - u_{pd} \right], -10 - u_{pd} \right] \\ u_{n+1} \leftarrow u_i + u_{pd} \end{array} \right. \\ \quad \left( \begin{array}{c} x \\ u \\ v \end{array} \right) \end{array}$$

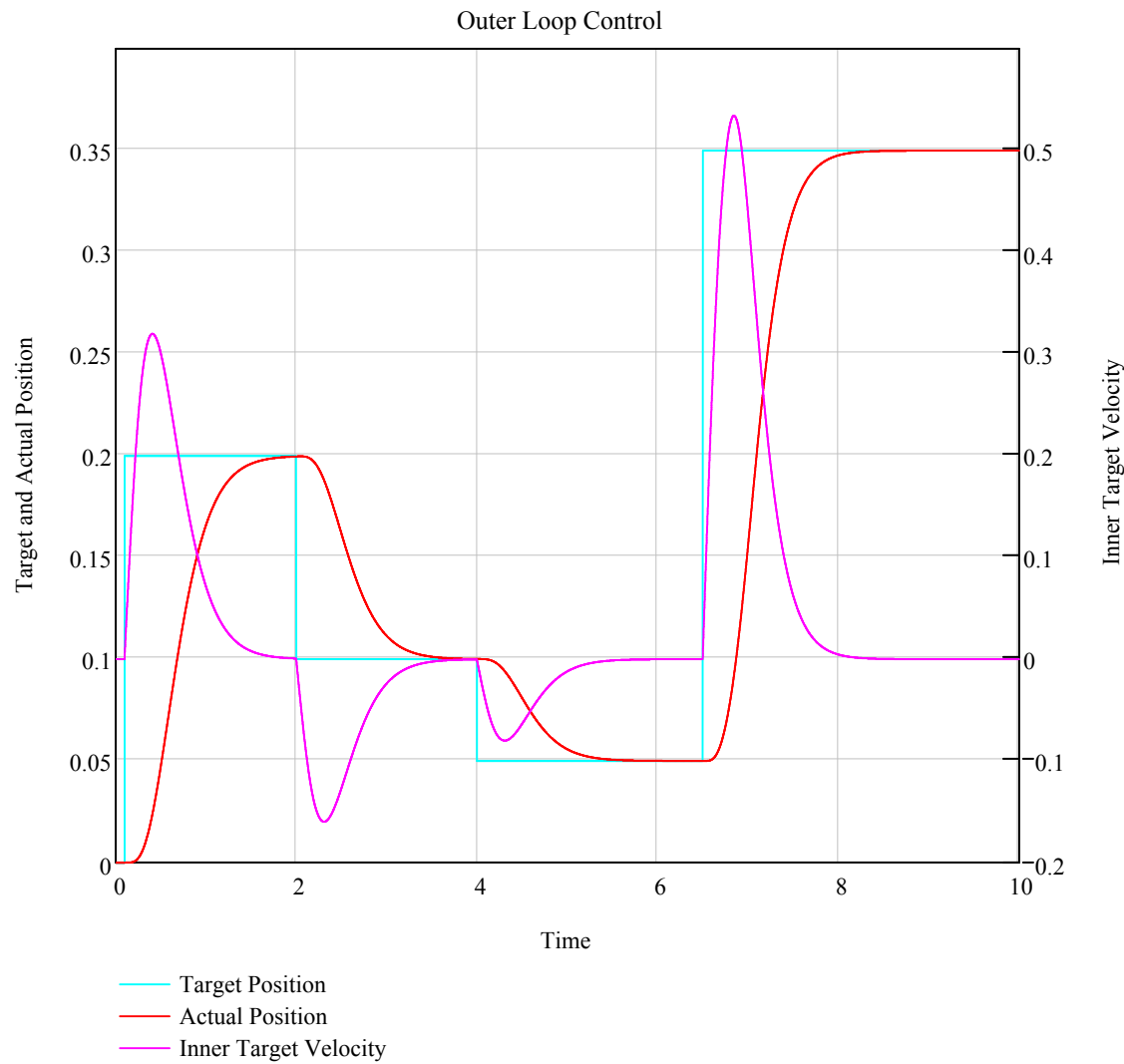

 $\begin{pmatrix} x \\ u \\ v \end{pmatrix} := \text{Cascade}(r)$ 

```

Compute the system response  
and control output

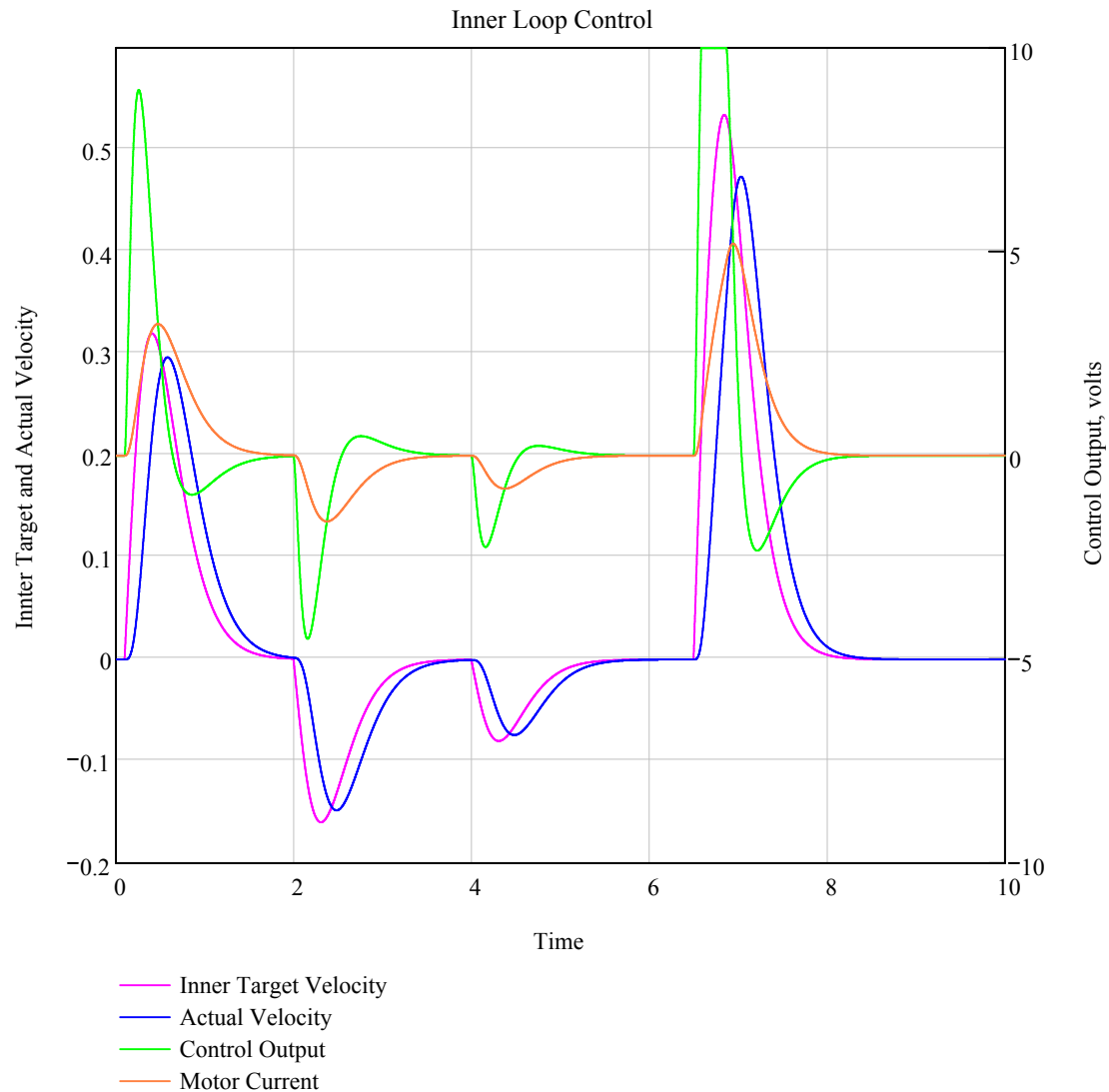
# DC Motor Speed Control

Verify By Simulating and Graphing the Results.



$K = 0.01$	$J = 0.01$	$R = 1$	$L = 0.5$	Motor
$\lambda = 18.849556$	$K_{i_1} = 3348.677881$	$K_{p_1} = 522.948638$	$K_{d_1} = 22.274334$	Inner Loop
$\mu = 6.692554$	$K_{i_0} = 8.92003$	$K_{p_0} = 5.630862$	$K_{d_0} = 0.373939$	Outer Loop

# DC Motor Speed Control



$K = 0.01$	$J = 0.01$	$R = 1$	$L = 0.5$	Motor
$\lambda = 18.849556$	$K_{i_1} = 3348.677881$	$K_{p_1} = 522.948638$	$K_{d_1} = 22.274334$	Inner Loop
$\mu = 6.692554$	$K_{i_0} = 8.92003$	$K_{p_0} = 5.630862$	$K_{d_0} = 0.373939$	Outer Loop

# DC Motor Speed Control

## Cascade Control of a Type 1 Single Pole System Following a Sine Wave

Amp := 0.5      Hz := 0.25

Amplitude and frequency of target generator.

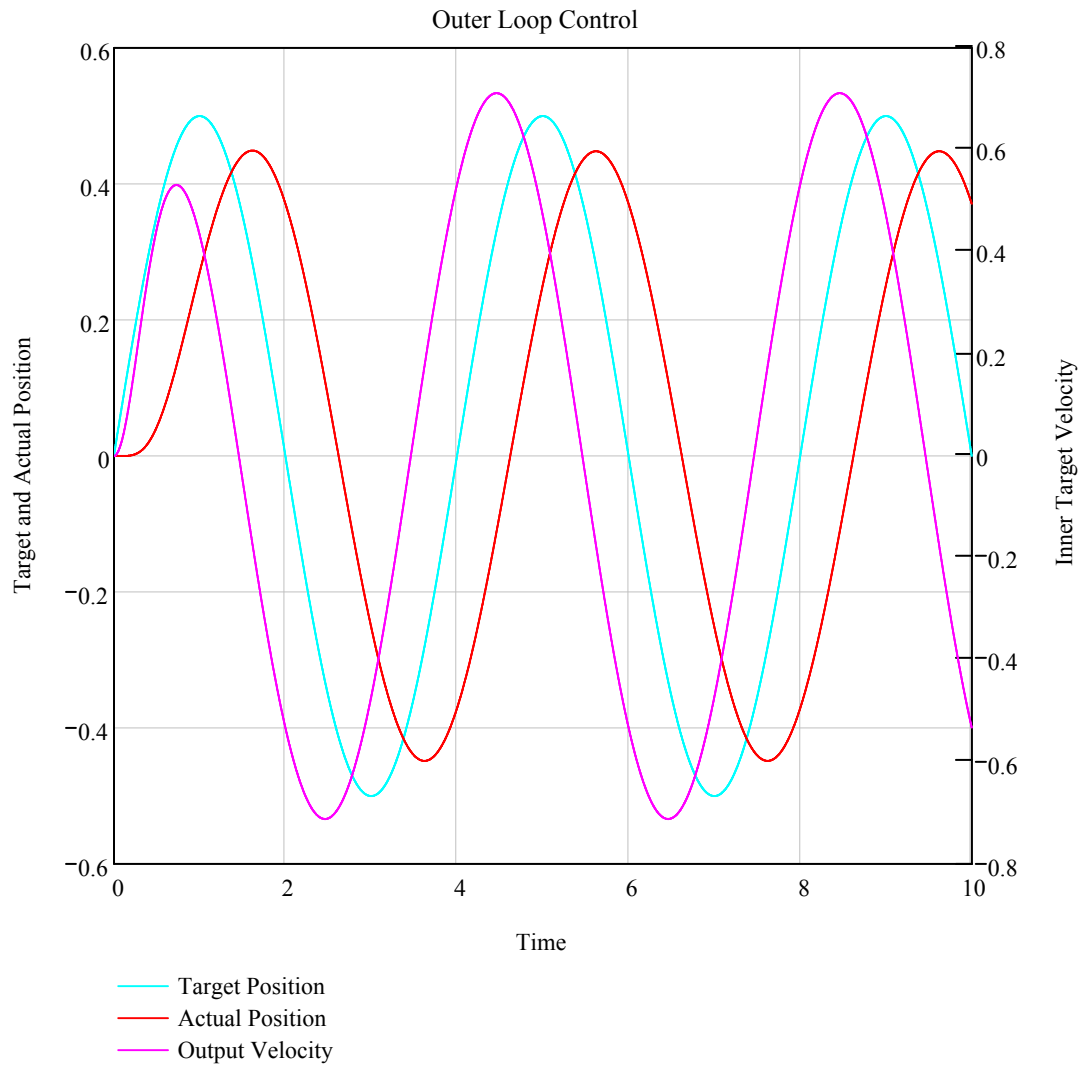
Initial state of position and velocity

$$r_n := \begin{pmatrix} \text{Amp} \cdot \sin(2 \cdot \pi \cdot \text{Hz} \cdot n \cdot T) \\ 2 \cdot \pi \cdot \text{Hz} \cdot \text{Amp} \cdot \cos(2 \cdot \pi \cdot \text{Hz} \cdot n \cdot T) \end{pmatrix}$$

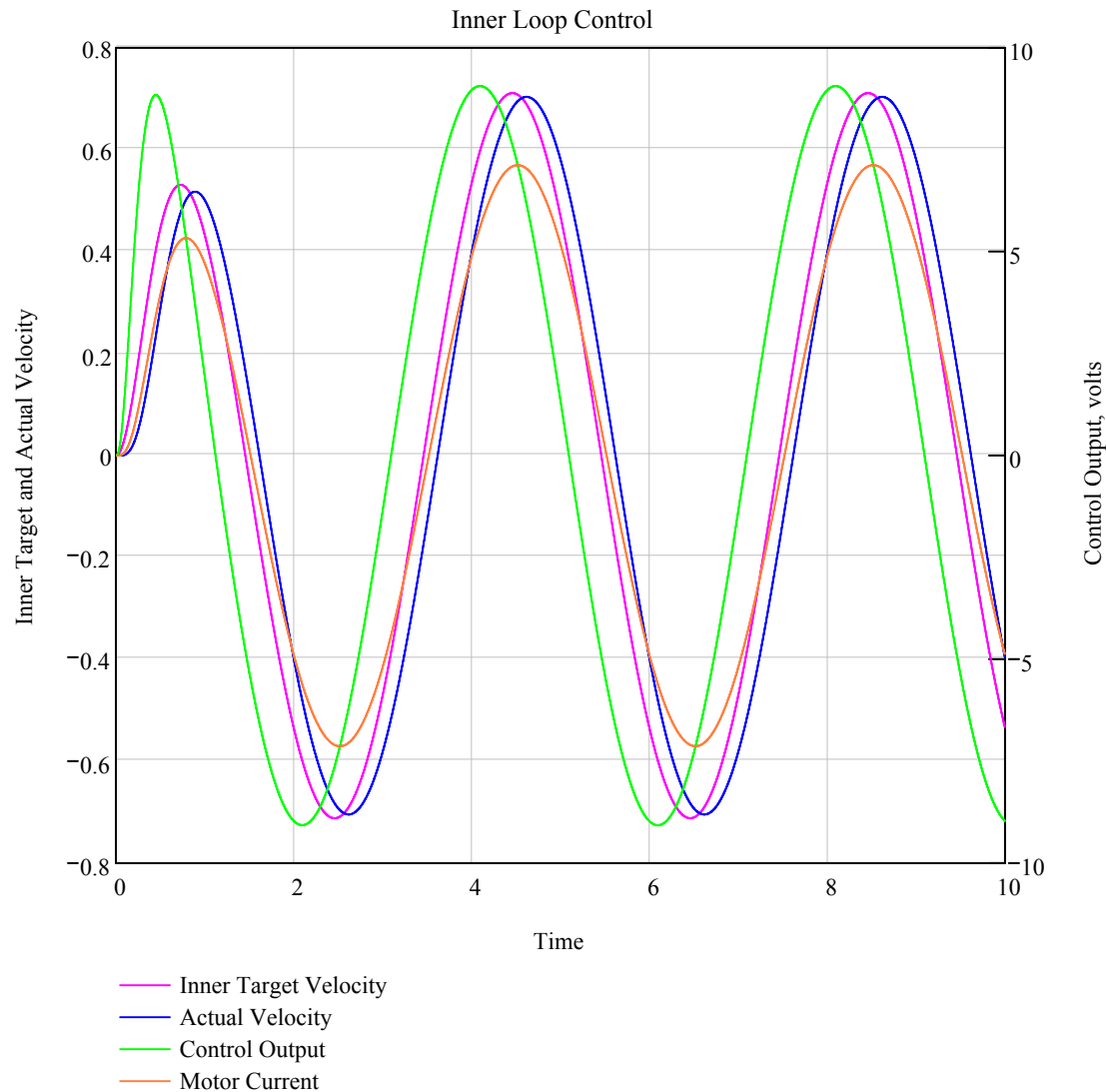
Sinusoidal motion generator.  
Generates target position, velocity and acceleration.

$$\begin{pmatrix} x \\ u \\ v \end{pmatrix} := \text{Cascade}(r)$$

Compute the system response and control output



# DC Motor Speed Control



$K = 0.01$	$J = 0.01$	$R = 1$	$L = 0.5$	Actuator
$\lambda = 18.849556$	$K_{i_1} = 3348.677881$	$K_{p_1} = 522.948638$	$K_{d_1} = 22.274334$	Inner Loop
$\mu = 6.692554$	$K_{i_0} = 8.92003$	$K_{p_0} = 5.630862$	$K_{d_0} = 0.373939$	Outer Loop

# DC Motor Speed Control

## Calculate Bandwidths

### Calculate Inner Loop Bandwidth

$$f(\omega) := \left| \frac{\left( \frac{K_i}{j \cdot \omega} \right) \cdot \frac{K}{[J \cdot (j \cdot \omega) + b] \cdot [L \cdot (j \cdot \omega) + R] + K^2}}{1 + \left[ \frac{K_i}{j \cdot \omega} + K p_i + K d_i \cdot (j \cdot \omega) \right] \cdot \frac{K}{[J \cdot (j \cdot \omega) + b] \cdot [L \cdot (j \cdot \omega) + R] + K^2}} \right|$$

$$\omega_i := 0.7 \cdot \lambda$$

$$\omega_i = 13.194689$$

The initial guess for the inner loop bandwidth

$$\omega_i := \text{root} \left( f(\omega_i) - \frac{1}{\sqrt{2}}, \omega_i \right) \quad \omega_i = 9.609966$$

Inner loop bandwidth in radians per second

$$\frac{\omega_i}{2 \cdot \pi} = 1.529474$$

Inner loop bandwidth in Hz

### Calculate Outer Loop Bandwidth

$$f(\omega) := \left| \frac{\left( \frac{K_i}{j \cdot \omega} \right) \cdot \frac{1}{j \cdot \omega} \cdot \frac{\left( \frac{K_i}{j \cdot \omega} \right) \cdot \frac{K}{[J \cdot (j \cdot \omega) + b] \cdot [L \cdot (j \cdot \omega) + R] + K^2}}{1 + \left[ \frac{K_i}{j \cdot \omega} + K p_i + K d_i \cdot (j \cdot \omega) \right] \cdot \frac{K}{[J \cdot (j \cdot \omega) + b] \cdot [L \cdot (j \cdot \omega) + R] + K^2}}}{1 + \left[ \frac{K_i}{j \cdot \omega} + K p_o + K d_o \cdot (j \cdot \omega) \right] \cdot \frac{1}{j \cdot \omega} \cdot \frac{\left( \frac{K_i}{j \cdot \omega} \right) \cdot \frac{K}{[J \cdot (j \cdot \omega) + b] \cdot [L \cdot (j \cdot \omega) + R] + K^2}}{1 + \left[ \frac{K_i}{j \cdot \omega} + K p_i + K d_i \cdot (j \cdot \omega) \right] \cdot \frac{K}{[J \cdot (j \cdot \omega) + b] \cdot [L \cdot (j \cdot \omega) + R] + K^2}}}$$

$$\omega_o := 0.2 \lambda$$

$$\omega_o = 3.769911$$

Initial guess for the outer loop band width

$$\omega_o := \text{root} \left( f(\omega_o) - \frac{1}{\sqrt{2}}, \omega_o \right) \quad \omega_o = 2.889634$$

Outer loop bandwidth in radians per second

$$\frac{\omega_o}{2 \cdot \pi} = 0.459899$$

outer loop bandwidth in Hz

$$\frac{\omega_i}{\omega_o} = 3.325669$$

Ratio of the inner loop to outer loop bandwidth. This ratio is fixed

# DC Motor Speed Control

## Inner Loop Bode Plot Calculations

$$T(s) := \frac{\left(\frac{K_i}{s}\right) \cdot \frac{K}{(J \cdot s + b) \cdot (L \cdot s + R) + K^2}}{1 + \left(\frac{K_i}{s} + K_p + K_d \cdot s\right) \cdot \frac{K}{(J \cdot s + b) \cdot (L \cdot s + R) + K^2}}$$

$n := 0..320$

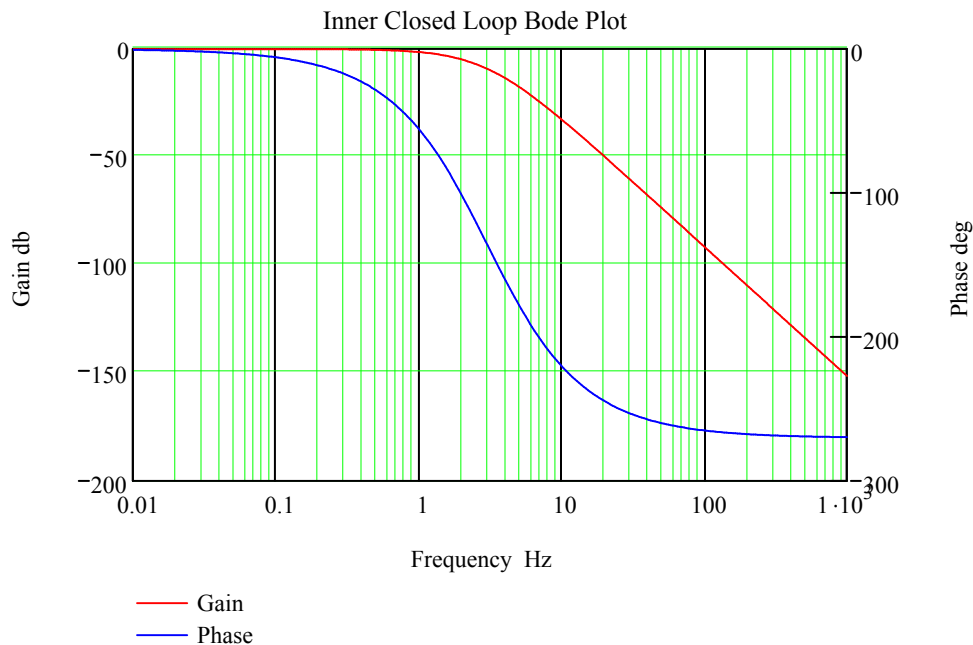
$$hz_n := 10^{\frac{n}{64}-2}$$

$$\begin{pmatrix} M_n \\ \phi_n \end{pmatrix} := \begin{cases} r \leftarrow T[j \cdot (2 \cdot \pi) \cdot hz_n] \\ a \leftarrow \frac{\arg(r)}{\deg} \\ a \leftarrow a - 360 \text{ if } n > 0 \wedge |a - \phi_{n-1}| > 100 \\ \begin{pmatrix} 20 \cdot \log(|r|) \\ a \end{pmatrix} \end{cases}$$

$K_p$  and  $K_d$  are in the feed back path only. This makes the inner loop less susceptible to the noisy target velocities generated by the outer loop.

Iterate the frequency from .01 HZ to 1000 HZ using 64 steps per decade for a total of 320 iterations.

Closed loop magnitude and phase as a function of frequency



# DC Motor Speed Control

## Outer Loop Bode Plot Calculations

$$T(s) := \frac{\left(\frac{K_{i_o}}{s}\right) \cdot \frac{\lambda^3}{s \cdot (s + \lambda)^3}}{1 + \left(\frac{K_{i_o}}{s} + K_{p_o} + K_{d_o} \cdot s\right) \cdot \frac{\lambda^3}{s \cdot (s + \lambda)^3}}$$

The outer loop gains are in the forward and feedback path. This help makes the outer loop faster than the inner loop.

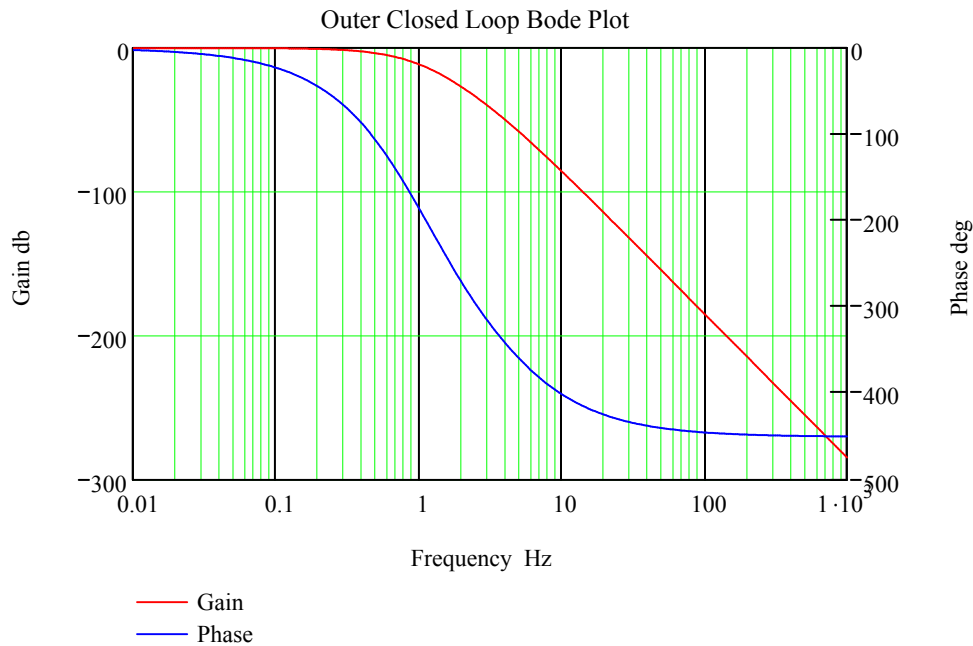
$n := 0..320$

$hz_n := 10^{\frac{n}{64}-2}$

Iterate the frequency from .01 HZ to 1000 HZ using 64 steps per decade for a total of 320 iterations.

$$\begin{pmatrix} M_n \\ \phi_n \end{pmatrix} := \begin{cases} r \leftarrow T[j \cdot (2 \cdot \pi) \cdot hz_n] \\ a \leftarrow \frac{\arg(r)}{\deg} \\ a \leftarrow a - 360 \text{ if } n > 0 \wedge |a - \phi_{n-1}| > 100 \\ \begin{pmatrix} 20 \cdot \log(|r|) \\ a \end{pmatrix} \end{cases}$$

Closed loop magnitude and phase as a function of frequency





# DC Motor Speed Control

Graph the Outer Loop Poles and Zeros

$$\lambda = 18.849556 \quad K_{i1} = 3348.677881 \quad K_{p1} = 522.948638 \quad K_{d1} = 22.274334$$

$$\mu = 6.692554 \quad K_{i0} = 8.92003 \quad K_{p0} = 5.630862 \quad K_{d0} = 0.373939$$

$$T_i(s) := \frac{(K_i + K_p \cdot s + K_d \cdot s^2) \cdot K}{J \cdot s^3 \cdot L + J \cdot s^2 \cdot R + b \cdot L \cdot s^2 + s \cdot b \cdot R + s \cdot K^2 + K \cdot K_i + K \cdot K_n \cdot s + K \cdot K_d \cdot s^2} \left| \begin{array}{l} \text{simplify} \\ \text{explicit} \end{array} \right. \rightarrow (K_i + K_p \cdot s + K_d \cdot s^2) \cdot K$$

$$T_o(s) := \frac{\left( \frac{K_{i0}}{s} \right) \cdot \frac{1}{s} \cdot \frac{(K_{i1} + K_{p1} \cdot s + K_{d1} \cdot s^2) \cdot K}{J \cdot s^3 \cdot L + (J \cdot R + b \cdot L + K \cdot K_{d1}) \cdot s^2 + (K^2 + K \cdot K_{p1} + b \cdot R) \cdot s + K \cdot K_{i1}}}{1 + \left( \frac{K_{i0}}{s} + K_{p0} + K_{d0} \cdot s \right) \cdot \frac{1}{s} \cdot \frac{(K_{i1} + K_{p1} \cdot s + K_{d1} \cdot s^2) \cdot K}{J \cdot s^3 \cdot L + (J \cdot R + b \cdot L + K \cdot K_{d1}) \cdot s^2 + (K^2 + K \cdot K_{p1} + b \cdot R) \cdot s + K \cdot K_{i1}}}$$

$$A_i := \text{denom}(T_i(s)) \left| \begin{array}{l} \text{coeffs, s} \\ \text{float, 7} \end{array} \right. \rightarrow \begin{pmatrix} 33.48679 \\ 5.329588 \\ .2827434 \\ .5e-2 \end{pmatrix}$$

$$A_o := \text{denom}(T_o(s)) \left| \begin{array}{l} \text{coeffs, s} \\ \text{float, 7} \end{array} \right. \rightarrow \begin{bmatrix} (-.840693) \cdot \lambda^5 \\ (-.1312876) \cdot \lambda^5 - 10.00339 \cdot \lambda^4 \\ (-1.562186) \cdot \lambda^4 - .559203e-2 \cdot \lambda^5 - 46.00881 \cdot \lambda^3 \\ (-7.285097) \cdot \lambda^3 - .6653937e-1 \cdot \lambda^4 \\ (-.3660357) \cdot \lambda^3 \\ (-.5e-2) \cdot \lambda^3 \end{bmatrix}$$

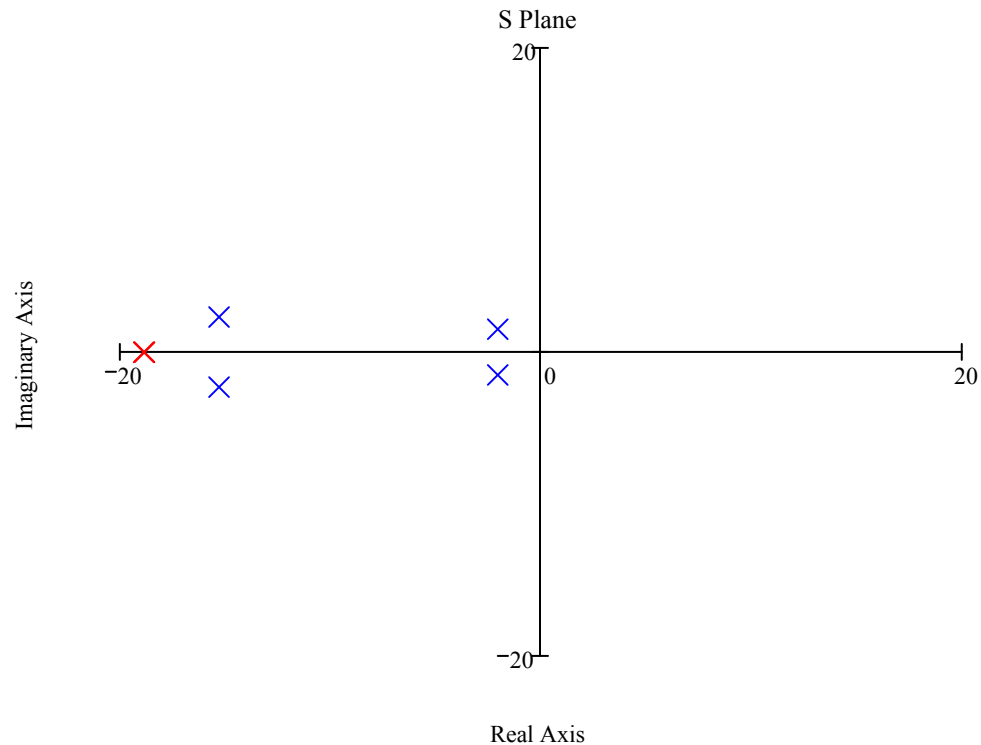
$$B_o := \text{numer}(T_o(s)) \left| \begin{array}{l} \text{coeffs, s} \\ \text{float, 6} \end{array} \right. \rightarrow \begin{bmatrix} (-.84070) \cdot \lambda^5 \\ (-.131287) \cdot \lambda^5 \\ (-.559199e-2) \cdot \lambda^5 \end{bmatrix}$$

$$\text{poles}_i := \text{polyroots}(A_i)$$

$$\text{poles}_o := \text{polyroots}(A_o)$$

$$\text{poles}_i = \begin{pmatrix} -18.862727 \\ -18.845535 \\ -18.840418 \end{pmatrix} \quad \text{poles}_o = \begin{pmatrix} -38.497281 \\ -15.302026 - 2.312133i \\ -15.302026 + 2.312133i \\ -2.052903 + 1.505003i \\ -2.052903 - 1.505003i \end{pmatrix}$$

# DC Motor Speed Control



×× Inner Loop Poles  
×× Outer Loop Poles

$K = 0.01$	$J = 0.01$	$R = 1$	$L = 0.5$	Motor
$\lambda = 18.849556$	$K_{i_1} = 3348.677881$	$K_{p_1} = 522.948638$	$K_{d_1} = 22.274334$	Inner Loop
$\mu = 6.692554$	$K_{i_0} = 8.92003$	$K_{p_0} = 5.630862$	$K_{d_0} = 0.373939$	Outer Loop

## DC Motor Speed Control

$$\frac{\mu^3 - 9\mu\lambda^2}{2} \cdot \mu + \frac{3}{2} \cdot \lambda - \frac{1}{2} \cdot \left[ (-15) \cdot \mu^2 + 18 \cdot \mu \cdot \lambda - 3 \cdot \lambda^2 \right]^{\frac{1}{2}} \cdot \frac{-3}{2} \cdot \mu + \frac{3}{2} \cdot \lambda + \frac{1}{2} \cdot \left[ (-15) \cdot \mu^2 + 18 \cdot \mu \cdot \lambda - 3 \cdot \lambda^2 \right]^{\frac{1}{2}}$$

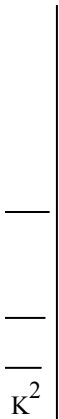
$$\frac{\mu^3 - 9\mu\lambda^2}{2} \cdot \mu + \frac{3}{2} \cdot \lambda + \frac{1}{2} \cdot \left[ (-15) \cdot \mu^2 + 18 \cdot \mu \cdot \lambda - 3 \cdot \lambda^2 \right]^{\frac{1}{2}} \cdot \frac{-3}{2} \cdot \mu + \frac{3}{2} \cdot \lambda - \frac{1}{2} \cdot \left[ (-15) \cdot \mu^2 + 18 \cdot \mu \cdot \lambda - 3 \cdot \lambda^2 \right]^{\frac{1}{2}}$$

## DC Motor Speed Control

$$\begin{bmatrix}
 3 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^3 \left[ \frac{-4}{5} + \frac{3}{10} \cdot 6^{\frac{1}{2}} + 2 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 \right] \cdot \lambda^2 \\
 3 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 \left[ 5 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 - \frac{9}{5} + \frac{4}{5} \cdot 6^{\frac{1}{2}} \right] \cdot \lambda \\
 10 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^3 - 18 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 + \frac{22}{5} - \frac{9}{10} \cdot 6^{\frac{1}{2}} \\
 \left( \frac{3}{5} + \frac{3}{20} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda - \frac{1}{2} \cdot \left[ (-3) \cdot \lambda^2 + 18 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda^2 - 15 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 \cdot \lambda^2 \right]^{\frac{1}{2}} \\
 \left( \frac{3}{5} + \frac{3}{20} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda + \frac{1}{2} \cdot \left[ (-3) \cdot \lambda^2 + 18 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right) \cdot \lambda^2 - 15 \cdot \left( \frac{3}{5} - \frac{1}{10} \cdot 6^{\frac{1}{2}} \right)^2 \cdot \lambda^2 \right]^{\frac{1}{2}}
 \end{bmatrix}$$

# DC Motor Speed Control

# DC Motor Speed Control



## DC Motor Speed Control

$$\left[ d \cdot s^2 \right) \cdot \frac{K}{J \cdot s^3 \cdot L + J \cdot s^2 \cdot R + b \cdot L \cdot s^2 + s \cdot b \cdot R + s \cdot K^2 + K \cdot K_i + K \cdot K_p \cdot s + K \cdot K_d \cdot s^2}$$

$$\begin{array}{l} \text{--} \left| \begin{array}{l} \text{simplify} \\ \text{collect, } s \rightarrow K \cdot (K_i + K_p \cdot s + K_d \cdot s^2) \\ \text{explicit} \end{array} \right. \cdot \frac{K \cdot (K_i + K_p \cdot s + K_d \cdot s^2)}{s^5 \cdot J \cdot L + (K \cdot K_d + J \cdot R + b \cdot L + K \cdot K_d \cdot K_d) \cdot s^4 + (K \cdot K_d \cdot K_p + K \cdot K_d \cdot K_i) \cdot s^3 + K \cdot K_d \cdot K_i \cdot s^2 + K \cdot K_d \cdot K_i \cdot s + K \cdot K_d \cdot K_i} \\ \text{--} \\ \text{i} \end{array}$$

## DC Motor Speed Control

$$\begin{bmatrix} \frac{1}{2} \\ \lambda^2 \end{bmatrix}$$



## DC Motor Speed Control

$$\frac{K_{i_o}}{\zeta \cdot K_{p_o} \cdot K_{d_i} + K \cdot K_{p_i} + b \cdot R + K^2} \cdot s^3 + (K \cdot K_{i_o} \cdot K_{d_i} + K \cdot K_{p_o} \cdot K_{p_i} + K \cdot K_{d_o} \cdot K_{i_i} + K \cdot K_{i_i}) \cdot s^2 + (K \cdot K_{i_o} \cdot K_{p_i} + K \cdot K_{p_o} \cdot K_{i_i} + K \cdot K_{d_o} \cdot K_{d_i} + K \cdot K_{i_i} \cdot K_{d_i}) \cdot s + K \cdot K_{i_o} \cdot K_{d_i} + K \cdot K_{p_o} \cdot K_{p_i} + K \cdot K_{d_o} \cdot K_{i_i} + K \cdot K_{i_i}$$

## DC Motor Speed Control

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$$\zeta \cdot K_{p0} \cdot K_{i1}) \cdot s + K \cdot K_{i0} \cdot K_{i1}$$